

MEE5114 Advanced Control for Robotics

Lecture 8: Rigid Body Dynamics

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Outline

- Spatial Acceleration
- Spatial Force (Wrench)
- Spatial Momentum
- Newton-Euler Equation using Spatial Vectors

Spatial Acceleration

- Given a rigid body with spatial velocity $\mathcal{V} = (\omega, v_o)$, its spatial acceleration is

coordinate-free \rightarrow

$$A = \dot{\mathcal{V}} = \begin{bmatrix} \dot{\omega} \\ \dot{v}_o \end{bmatrix}, \quad \mathcal{A} = \lim_{\delta \rightarrow 0} \frac{\mathcal{V}(t+\delta) - \mathcal{V}(t)}{\delta}$$

- Recall that: v_o is the velocity of the body-fixed particle coincident with frame origin o at the current time t .

- Note: $\dot{\omega}$ is the angular acceleration of the body

$$v_o = \dot{q}(t), \text{ for some body-fixed pt}$$

- \dot{v}_o is not the acceleration of any body-fixed point! but $\dot{v}_o \neq \ddot{q}(t)$

- In fact, \dot{v}_o gives the rate of change in stream velocity of body-fixed particles passing through o

Spatial vs. Conventional Accel. (1/2)

- Why " \dot{v}_o is not the acceleration of any body-fixed point"?
- Suppose $q(t)$ is the body fixed particle coincides with o at time t_o
- So by definition, we have $v_o(t_o) = \dot{q}(t_o)$, however, $\dot{v}_o(t_o) \neq \ddot{q}(t_o)$, where $\ddot{q}(t)$ is the conventional acceleration of the body-fixed point q

$$q(t_o) = "o"$$

- Note: $\dot{v}_o(t_o) \stackrel{\Delta}{=} \lim_{\delta \rightarrow 0} \frac{v_o(t_o + \delta) - v_o(t_o)}{\delta} \neq \dot{q}(t_o)$

$\swarrow q_1(t_o + \delta) \neq q(t_o + \delta)$
 $\swarrow q(t_o)$

At time $t = t_o$, $q(t_o) = o$, $v_o(t_o) = \dot{q}(t_o)$

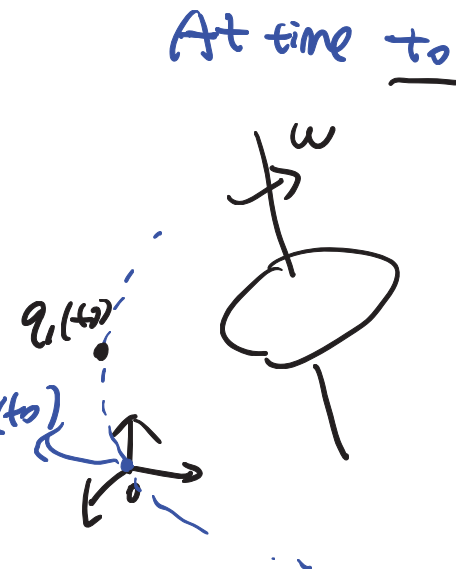
time $t = t_o + \delta$, $q_1(t_o + \delta) \neq o$, $v_o(t_o + \delta) \neq \dot{q}(t_o + \delta)$

\nwarrow another body-fixed particle

$$= q_1(t_o + \delta) \quad q(t_o)$$

Note: q_1 and q are different joints

$$q_1(t_o + \delta) \neq q(t_o + \delta)$$



Spatial vs. Conventional Accel. (2/2)

$$\frac{v(t_0 + \delta) - v(t_0)}{\delta} \neq \frac{\dot{q}(t_0 + \delta) - \dot{q}(t_0)}{\delta} \xrightarrow{\delta \rightarrow 0} \ddot{q}(t_0)$$

By definition:

$$\dot{q}(t) = v_o(t) + \omega(t) \times q(t) \leftarrow \text{holds for all } t$$

$$\ddot{q}(t) = \dot{v}_o(t) + \dot{\omega}(t) \times q(t) + \omega(t) \times \dot{q}(t) \leftarrow \checkmark$$

At $t = t_0$,
if $q(t_0) = 0$

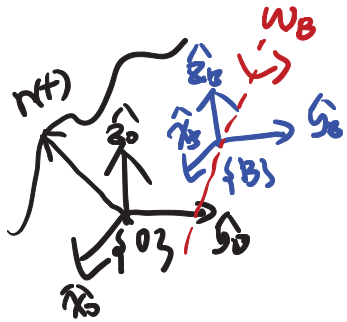
$$\dot{q}(t_0) = \dot{v}_o(t_0) + \omega(t_0) \times \dot{q}(t_0)$$

- If $q(t)$ is the body fixed particle coincides with o at time t , then we have

$$\ddot{q}(t) = \dot{v}_o(t) + \omega(t) \times \dot{q}(t)$$

Plücker Coordinate System and Basis Vectors (1/2)

- Recall coordinate-free concept: let $\overset{r}{r} \in \mathbb{R}^3$ be a free vector with $\{o\}$ and $\{B\}$ frame coordinate ${}^o r$ and B_r



$${}^o r = \begin{bmatrix} {}^o r_x \\ {}^o r_y \\ {}^o r_z \end{bmatrix} \in \mathbb{R}^3 \iff \overset{r}{r} = [\hat{x}_o \ \hat{y}_o \ \hat{z}_o] \overset{o}{r} \dots \textcircled{1}$$

$$B_r = \begin{bmatrix} B_{r_x} \\ B_{r_y} \\ B_{r_z} \end{bmatrix} \in \mathbb{R}^3 \iff \overset{r}{r} = [\hat{x}_B \ \hat{y}_B \ \hat{z}_B] \overset{B}{r} \dots \textcircled{2}$$

$$\textcircled{1} \Rightarrow \dot{\overset{r}{r}} = [\hat{x}_o \ \hat{y}_o \ \hat{z}_o] \frac{d}{dt}(\overset{o}{r})$$

express this "physics" using $\{o\}$

$$\Rightarrow \overset{o}{r} = [\overset{o}{\hat{x}}_B \ \overset{o}{\hat{y}}_B \ \overset{o}{\hat{z}}_B] B_r$$

apparent derivative

$$\stackrel{\text{apparent}}{=} \overset{o}{\dot{r}}$$

${}^o R_B \leftarrow$ change of coord

use $\{o\}$ -frame to express:

$$\overset{o}{\dot{r}} = [\overset{o}{\hat{x}}_B \ \overset{o}{\hat{y}}_B \ \overset{o}{\hat{z}}_B] \frac{d}{dt}(\overset{o}{r})$$

$$\overset{o}{\dot{r}} = \frac{d}{dt}(\overset{o}{r})$$

$I_{3 \times 3}$

Plücker Coordinate System and Basis Vectors (2/2)

• ② $\Rightarrow r = [\hat{x}_B \ \hat{y}_B \ \hat{z}_B]^B r \quad \dot{\hat{x}}_B = \omega_B \times \hat{x}_B$

$(\dot{r} \neq \frac{d}{dt}({}^B r) \quad \times)$

$$\begin{aligned} \Rightarrow \dot{r} &= \underbrace{[\dot{\hat{x}}_B \ \dot{\hat{y}}_B \ \dot{\hat{z}}_B]}_{\omega_B \times [\hat{x}_B \ \hat{y}_B \ \hat{z}_B]} {}^B r + [\hat{x}_B \ \hat{y}_B \ \hat{z}_B] \frac{d}{dt}({}^B r) \\ &= \omega_B \times [\hat{x}_B \ \hat{y}_B \ \hat{z}_B] {}^B r + \left[\checkmark \right] \frac{d}{dt}({}^B r) \dots \end{aligned}$$

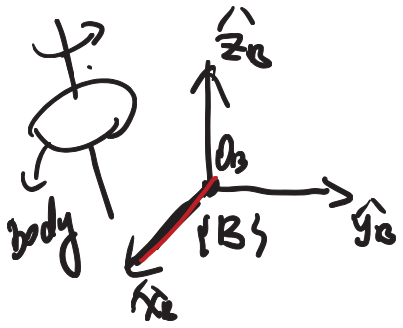
use $\{B\}$ frame to express the above equ.

$$\textcircled{{}^B \dot{r}} = \underbrace{{}^B \omega_B \times {}^B r}_{\downarrow \text{accounts for coordinate frame axes is moving}} + \textcircled{\frac{d}{dt}({}^B r)} \xrightarrow{\text{due to changes in coordinate}} {}^B \dot{r}^0$$

$${}^B \left(\frac{d}{dt}({}^B r) \right)_{B_j}$$

accounts for coordinate frame axes is moving

due to changes in coordinate



${}^B v_{\text{body}} = \begin{bmatrix} 1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$, means rotating about \hat{x}_B at unit speed
 $\Leftrightarrow v_{\text{body}} = \underline{e_{B1}}$ motion basis vector

Given $\{B\}$ frame

$\{e_{B1}, e_{B2}, \dots, e_{B6}\}$ - 6dim

motion basis vectors

coordinate free

$\begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$, $v_{\text{body}} = e_{B2}$ \hat{x}_B

$\begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$, linear motion along \hat{x}_B at unit speed

$v_{\text{body}} = \alpha_1 e_{B1} + \alpha_2 e_{B2} + \dots + \alpha_6 e_{B6}$, where $\begin{bmatrix} \alpha_1 \\ \alpha_2 \\ \vdots \\ \alpha_6 \end{bmatrix} = {}^B v_{\text{body}}$

use $\{o\}$ frame to represent above "physics"

${}^o v_{\text{body}} = \alpha_1 {}^o e_{B1} + \alpha_2 {}^o e_{B2} + \dots + \alpha_6 {}^o e_{B6} = [{}^o e_{B1} \quad {}^o e_{B2} \quad \dots \quad {}^o e_{B6}] {}^B v_{\text{body}}$

${}^o e_{Bi}$: can be computed from "physics" and twist def.

unit speed rotation about $o_B \hat{x}_B$ expressed in $\{o\}$

$$- \underbrace{[{}^0e_{B_1} \quad {}^0e_{B_2} \quad \dots \quad {}^0e_{B_6}]}_{b \times b} = \underbrace{({}^0X_B)}_{b \times b} = \underbrace{[Ad_{T_B}]}_{b \times b}$$

$$\bullet \quad A_{body} = \frac{d}{dt}(\dot{V}_{body}) \quad ; \quad \underline{V_{body} = [e_{B_1} \quad \dots \quad e_{B_6}]^B \dot{V}_{body}}$$

$$\Rightarrow A_{body} = \frac{d}{dt}(\dot{V}_{body}) = \underbrace{[\dot{e}_{B_1} \quad \dot{e}_{B_2} \quad \dots \quad \dot{e}_{B_6}]}^B \dot{V}_{body} + [e_{B_1} \quad \dots \quad e_{B_6}] \underbrace{\frac{d}{dt}({}^B \dot{V}_{body})}_{{}^B \ddot{V}_{body}}$$

If $\{B\}$ - does not change.

$$\left. \begin{array}{l} \dot{V}_{body} = [e_{B_1} \quad \dots \quad e_{B_6}]^B \dot{V}_{body} \\ \text{special case: } {}^0A = {}^0 \dot{V}_{body} \end{array} \right\} \begin{array}{l} \text{express this in } \{B\} \\ \underbrace{{}^B(\dot{V}_{body})}_{{}^B A_{body}} = {}^B \dot{V}_{body} = \frac{d}{dt}({}^B V_{body}) \end{array}$$

If $\{B\}$ - changes over time, ${}^B A \neq {}^B \dot{V}_{body}$

Then the key is to compute $[\dot{e}_{B_1} \quad \dot{e}_{B_2} \quad \dots \quad \dot{e}_{B_6}]$ \leftarrow can be computed purely

Work with Moving Reference Frame

by physics (see featherstone)

- Now let's work with $\{B\}$ frame to find the derivative

$$\Rightarrow \text{we need to compute: } [{}^0\dot{e}_{B_1} \quad {}^0\dot{e}_{B_2} \quad \dots \quad {}^0\dot{e}_{B_6}] = {}^0\dot{X}_B = \frac{d}{dt} [Ad_{0T_B}]$$

let's denote: ${}^0T_B = (R, p) \Rightarrow \frac{d}{dt} \begin{pmatrix} R & 0 \\ [p]R & R \end{pmatrix} = \begin{pmatrix} \dot{R} & 0 \\ ([p]R)' & \dot{R} \end{pmatrix}$

$\{B\}$ -frame has instantaneous velocity $v_B = \begin{bmatrix} \omega \\ v \end{bmatrix}$

Note: $\dot{R} = \omega \times R$, $\dot{p} = v + \omega \times p$, $[R\omega] = R[\omega]R^T$
 $[\omega_1 \times \omega_2] = [\omega_1][\omega_2] - [\omega_2][\omega_1]$... Jacobi's identity

$$\Rightarrow \text{After some computation, } \frac{d}{dt} (Ad_{0T_B}) = \begin{bmatrix} [\omega] & 0 \\ [v] & [\omega] \end{bmatrix} (Ad_{0T_B})$$

$$\underbrace{{}^0\dot{X}_B}_{6 \times 6} = \underbrace{\begin{bmatrix} [\omega] & 0 \\ [v] & [\omega] \end{bmatrix}}_{6 \times 6} \underbrace{{}^0X_B}_{6 \times 6}$$

Define: $\begin{bmatrix} [w] & 0 \\ [v] & \dot{w} \end{bmatrix} \triangleq \left[\mathcal{V}_B \times \right]$, $\dot{X}_B = \mathcal{V}_B \times X_B$

$$\dot{R}_B = \omega_B \times R_B$$

In coordinate free: $\dot{e}_{B_1} = \mathcal{V}_B \times e_{B_1}$, $\dot{e}_{B_2} = \mathcal{V}_B \times e_{B_2} \dots$

Derivative of Adjoint

- Suppose a frame $\{A\}$'s pose is $T_A = (R_A, p_A)$, and is moving at an instantaneous velocity $\mathcal{V}_A = (\omega, v)$. Then

$$\frac{d}{dt}([\text{Ad}_{T_A}]) = \begin{bmatrix} [\omega] & \overset{0}{\cancel{[v]}} \\ [v] & \underset{\checkmark}{[S_\omega]} \end{bmatrix} [\text{Ad}_{T_A}]$$

$${}^0\dot{X}_A = \mathcal{V}_A \times {}^0X_A$$

$$\dot{X}_A = \mathcal{V}_A \times X_A$$

$${}^A\dot{X}_A = {}^A\mathcal{V}_A \times {}^AX_A$$

Spatial Cross Product

- Given two spatial velocities (twists) \mathcal{V}_1 and \mathcal{V}_2 , their spatial cross product is:

$$\mathcal{V}_1 \times \mathcal{V}_2 = \begin{bmatrix} \omega_1 \\ v_1 \end{bmatrix} \times \begin{bmatrix} \omega_2 \\ v_2 \end{bmatrix} \triangleq \begin{bmatrix} \omega_1 \times \omega_2 \\ \omega_1 \times v_2 + v_1 \times \omega_2 \end{bmatrix}$$

Lie Bracket

- Matrix representation: $\mathcal{V}_1 \times \mathcal{V}_2 = [\mathcal{V}_1 \times] \mathcal{V}_2$, where

$$[\mathcal{V}_1 \times] \triangleq \begin{bmatrix} [\omega_1] & 0 \\ [v_1] & [\omega_1] \end{bmatrix}$$

- Roughly speaking, when a motion vector \mathcal{V} is moving with a spatial velocity \mathcal{Z} (e.g. it is attached to a moving frame) but is otherwise not changing, then

$$\dot{\mathcal{V}} = \mathcal{Z} \times \mathcal{V}$$

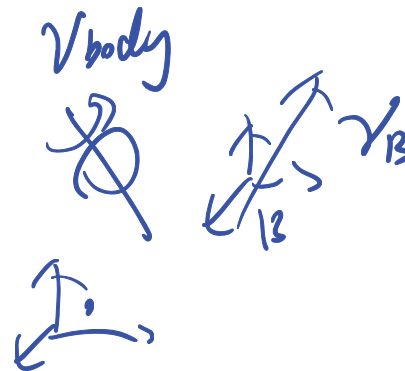
Spatial Cross Product: Properties (1/1)

- Assume A is moving wrt to O with velocity \mathcal{V}_A

$${}^o\dot{X}_A = [{}^o\mathcal{V}_A \times] {}^oX_A$$

- $[X\mathcal{V}\times] = X[\mathcal{V}\times]X^T$, for any transformation X and twist \mathcal{V}

$$[Rw] = R[w]R^T$$



Spatial Acceleration with Moving Reference Frame

Consider a body with velocity \mathcal{V}_{body} (wrt inertia frame), and ${}^O\mathcal{V}_{body}$ and ${}^B\mathcal{V}_{body}$ be its Plücker coordinates wrt $\{O\}$ and $\{B\}$:

- $${}^B\mathcal{A}_{body} = \underbrace{\frac{d}{dt} ({}^B\mathcal{V}_{body})}_{\text{apparent derivative}} + \underbrace{{}^B\mathcal{V}_B \times {}^B\mathcal{V}_{body}}_{\text{due to frame } \{B\} \text{ is moving}}$$

$${}^B \left(\frac{d}{dt} (\mathcal{V}_{body}) \right) = {}^B \dot{\mathcal{V}}_{body}$$

- $${}^O\mathcal{A} = {}^O X_B {}^B\mathcal{A} \leftarrow$$

$${}^O\mathcal{A}_{body} = \frac{d}{dt} ({}^O\mathcal{V}_{body}) = \frac{d}{dt} ({}^O X_B {}^B\mathcal{V}_{body}) = \underbrace{{}^O \dot{X}_B} {}^B\mathcal{V}_{body} + {}^O X_B {}^B \dot{\mathcal{V}}_{body}$$

$$= [{}^O\mathcal{V}_B \times] {}^O X_B {}^B\mathcal{V}_{body} + {}^O X_B {}^B \dot{\mathcal{V}}_{body}$$

$$= {}^O X_B \left(\underbrace{{}^B X_O [{}^O\mathcal{V}_B \times]}_{{}^B X_O [{}^O\mathcal{V}_B \times]} {}^O X_B {}^B\mathcal{V}_{body} + {}^B \dot{\mathcal{V}}_{body} \right) = {}^O X_B \left(\underbrace{{}^B \dot{\mathcal{V}}_{body} + {}^B\mathcal{V}_B \times {}^B\mathcal{V}_{body}}_{{}^B\mathcal{A}_{body}} \right)$$

$$[{}^B X_O [{}^O\mathcal{V}_B \times]] = [{}^B\mathcal{V}_B \times]$$

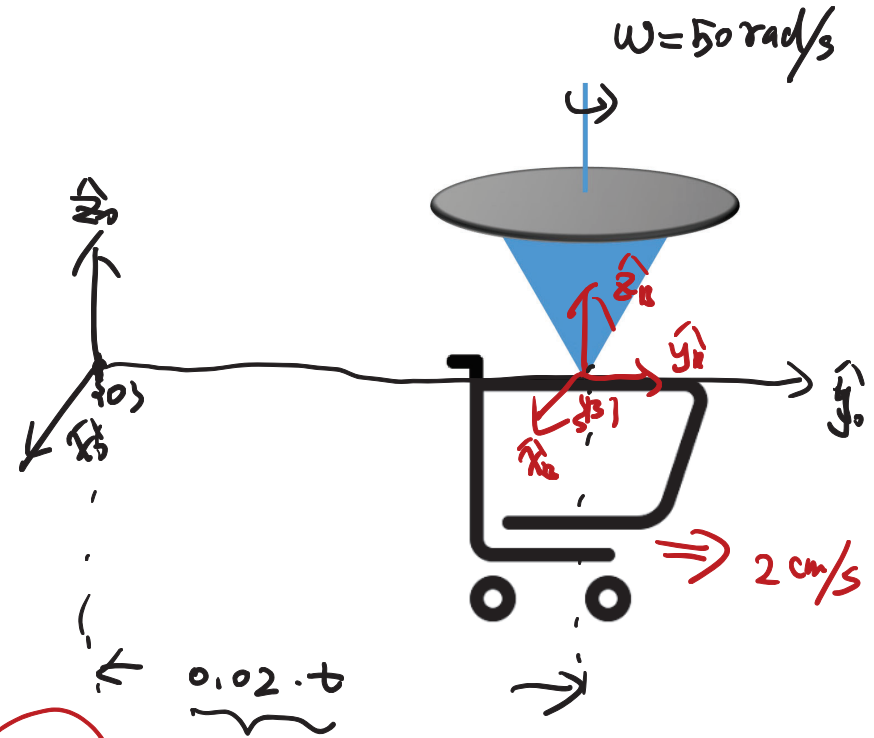
Spatial Acceleration Example

Find ${}^B A_{top}$

Method 1: ${}^B A_{top} = {}^B X_0 \cdot {}^0 A_{top} = {}^B X_0 \frac{d}{dt} ({}^0 v_{top})$

$${}^0 v_{top} = \begin{bmatrix} 0 \\ 0 \\ 50 \\ 50 \cdot (0.02t) \\ 0.02 \\ 0 \end{bmatrix}, \quad {}^0 A_{top} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

$${}^B A_{top} = {}^B X_0 \cdot {}^0 A_{top} = \begin{bmatrix} I & \\ & I \end{bmatrix} \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$



Method 2:

$${}^B v_{top} = \begin{bmatrix} 0 \\ 0 \\ 50 \\ 0 \\ 0.02 \\ 0 \end{bmatrix}$$

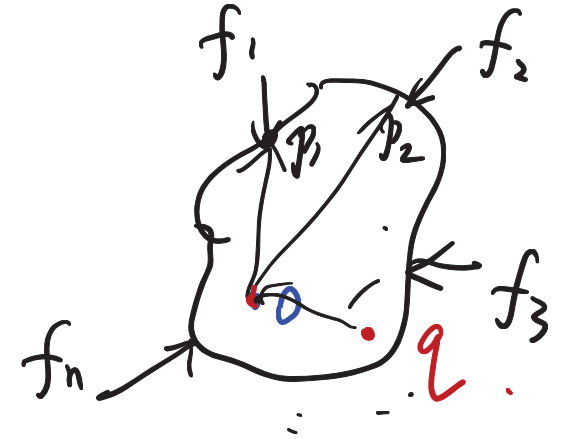
$${}^B A_{top} = \frac{d}{dt} ({}^B v_{top}) + {}^B v_{Bframe} \times {}^B v_{top} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0.02 \\ 0 \end{bmatrix} \times \begin{bmatrix} 0 \\ 0 \\ 50 \\ 0 \\ 0.02 \\ 0 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

Outline

- Spatial Acceleration
- Spatial Force (Wrench)
- Spatial Momentum
- Newton-Euler Equation using Spatial Vectors

Spatial Force (Wrench)

- Consider a rigid body with many forces on it and fix an arbitrary point O in space



- The net effect of these forces can be expressed as
 - A force f , acting along a line passing through O

$$f = \sum f_i$$

- A moment n_O about point O

$$n_O \in \mathbb{R}^3$$

$$n_O = \sum_i (\vec{OP}_i) \times f_i$$

- Spatial Force (Wrench):** is given by the 6D vector

$$\mathcal{F} = \begin{bmatrix} n_O \\ f \end{bmatrix}$$

$$V_q = V_o + \omega \times \vec{oq}$$

what if we change reference point to q

$$\begin{aligned} n_q &= \sum_i (\vec{qP}_i) \times f_i = n_O + \sum_i (\vec{qP}_i - \vec{OP}_i) \times f_i \\ &= n_O + \vec{qO} \times \sum_i f_i = n_O + \vec{qO} \times f \end{aligned}$$

Spatial Force in Plücker Coordinate Systems $= n_0 + f \times oq$

- Given a frame $\{A\}$, the Plücker coordinate of a spatial force \mathcal{F} is given by

$${}^B \mathcal{F} = \begin{bmatrix} {}^B n_{0B} \\ {}^B f \end{bmatrix}$$

$${}^A \mathcal{F} = \begin{bmatrix} {}^A n_{0A} \\ {}^A f \end{bmatrix}$$

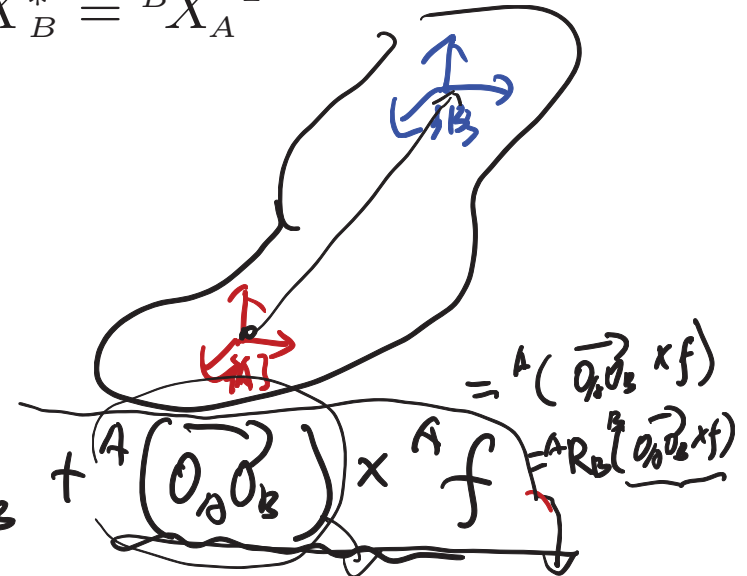
$${}^A T_B = ({}^A R_B, {}^A p_B)$$

- Coordinate transform: ${}^A \mathcal{F} = {}^A X_B^* {}^B \mathcal{F}$ where ${}^A X_B^* = {}^B X_A^T$

$$\boxed{{}^A f = {}^A R_B {}^B f} \quad \text{--- ①}$$

moment: $n_{0A} = n_{0B} + o_A o_B \times f$
 coord-free

choose $\{A\}$ -free t-express:



$$\begin{aligned} {}^A n_{0A} &= {}^A n_{0B} + {}^A (o_A o_B) \times {}^A f \\ &= {}^A R_B {}^B n_{0B} + {}^A R_B (-{}^B p_A \times {}^B f) \\ &= {}^A R_B {}^B n_{0B} - {}^A R_B [{}^B p_A] {}^B f \end{aligned} \quad \text{--- ②}$$

$$\begin{bmatrix} {}^A n_{0A} \\ {}^A f \end{bmatrix} = \begin{bmatrix} {}^A R_B & -{}^A R_B [{}^B p_A] \\ 0 & {}^A R_B \end{bmatrix} \begin{bmatrix} {}^B n_{0B} \\ {}^B f \end{bmatrix}$$

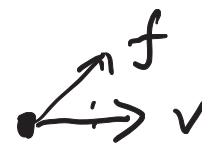
\Rightarrow

\triangleq $\begin{matrix} \swarrow \\ \overline{A} \times \overline{B}^* \\ \searrow \\ \text{~~~~~} \end{matrix}$

$\boxed{\overline{A} \times \overline{B}^* = (\overline{B} \times \overline{A})^T}$
 6×6

$$\overline{B} \times \overline{A} = \begin{bmatrix} \overline{B} R_A & 0 \\ \begin{bmatrix} \overline{B} R_A \\ \overline{B} R_A \end{bmatrix} & \overline{B} R_A \end{bmatrix}$$

Wrench-Twist Pair and Power



$$p = f^T v = \langle f, v \rangle$$

- Recall that for a point mass with linear velocity v and linear force f . Then we know that the power (instantaneous work done by f) is given by $f \cdot v = f^T v$
- This relation can be generalized to spatial force (i.e. wrench) and spatial velocity (i.e. twist)
- Suppose a rigid body has a twist ${}^A \mathcal{V} = ({}^A \underline{\omega}, {}^A \underline{v}_{O_A})$ and a wrench ${}^A \mathcal{F} = ({}^A n_{O_A}, {}^A f)$ acts on the body. Then the power is simply

$$\begin{aligned}
 \text{Scalar } \mathcal{P} &= \underbrace{({}^A \mathcal{V})^T}_{6 \times 1} \underbrace{{}^A \mathcal{F}}_{6 \times 1} = {}^A \mathcal{F}^T {}^A \mathcal{V} \\
 &= \underbrace{({}^A \omega)^T}_{\text{rotational}} \underbrace{{}^A n_{O_A}}_{\text{power}} + \underbrace{{}^A v_{O_A}^T}_{\text{power}} \underbrace{{}^A f}_{\text{power}}
 \end{aligned}$$

Joint Torque

- Consider a link attached to a 1-dof joint (e.g. revolute or prismatic). Let \hat{S} be the screw axis of the joint. The velocity of the link induced by joint motion is given by: $\underline{v} = \hat{S}\dot{\theta}$



- \mathcal{F} be the wrench provided by the joint. Then the power produced by the joint is

$$P = \underline{v}^T \mathcal{F} = \left[\hat{S}^T \mathcal{F} \right] \dot{\theta} \triangleq \tau \dot{\theta}$$

$\rightarrow (\hat{S}\dot{\theta})^T \mathcal{F} \rightarrow \triangleq \tau \text{ scalar}$

- $\tau = \hat{S}^T \mathcal{F} = \mathcal{F}^T \hat{S}$ is the projection of the wrench onto the screw axis, i.e. the effective part of the wrench.

- Often times, τ is referred to as joint "torque" or generalized force

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Rotational Inertia (1/2)

- Recall momentum for point mass:

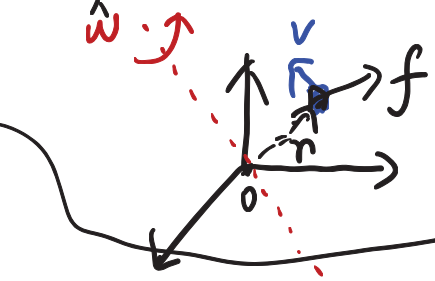
Linear

velocity: $v = \dot{r}, a = \dot{v} = \ddot{r} \in \mathbb{R}^3$

force: $f = ma = m\dot{v} = m\ddot{r}$

Linear momentum: $L = mv$

point mass: m



Rotational

$\omega = \hat{\omega} \dot{\theta}, v = \omega \times r$

moment: $n = r \times f$

$a \times b = -b \times a$

angular momentum: $\phi = r \times L$

$= r \times (m \omega \times r)$

$= m (r \times \omega \times r)$

$= m r \times (-r) \times \omega$

$= m \begin{bmatrix} r \\ -r \end{bmatrix} \omega \rightarrow I$

3x3 matrix

Inertia matrix for this point mass

Rotational Inertia (2/2) ^{density}

• Rotational Inertia: $\bar{I} \triangleq \int_{\mathcal{V}} \rho(r) [r][r]^T dr$

- $\rho(\cdot)$ is the density function of the body

- \bar{I} depends on coordinate system

- It is a constant matrix if the origin coincides with CoM

what's definition for CoM?

$$c \triangleq \text{CoM} = \frac{1}{m} \int \rho(r) \cdot r \, dV$$

$$c = \frac{1}{m} \sum m_i r_i$$

If c is CoM, then

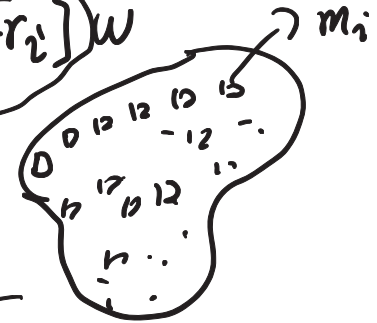
$$\frac{1}{m} \sum m_i (c \vec{r}_i) = 0$$

$$\boxed{\sum_i m_i (c \vec{r}_i) = 0} \Rightarrow \boxed{\sum_i m_i [c \vec{r}_i] = 0}$$

$$\phi = \left(\sum m_i [r_i] [r_i]^T \right) \omega$$

this matrix depends on coord sys

to represent r_i



$$[-r_i] = [r_i]^T$$

Spatial Momentum



- Consider a rigid body with spatial velocity $\mathcal{V}_C = (\omega, v_C)$ expressed at the center of mass C

- Linear momentum: $\mathcal{L} = m v_{com} = m v_C$ why? $L = \sum_i m_i v_i = \sum_i m_i (v_C + \omega \times r_i)$

$$= (\sum_i m_i) v_C + \left(\sum_i m_i (r_i) \right) \times \omega$$

- Angular momentum about CoM: $\phi_C = \bar{I}_C \omega$; $\phi_C = \sum_i r_i \times m_i v_i = \sum_i r_i \times (m_i v_C + m_i \omega \times r_i)$

$$= \left(\sum_i r_i \times m_i v_C \right) + \sum_i m_i r_i \times \omega \times r_i$$

- Angular momentum about a point O :

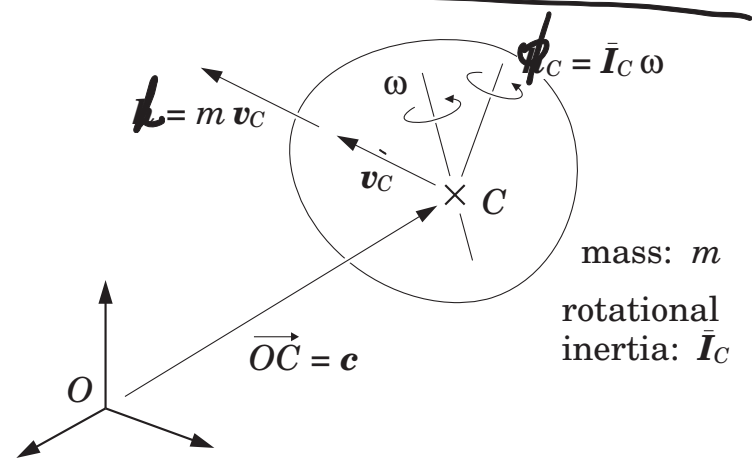
$$\phi_O = \sum_i \vec{O}r_i \times (m_i v_i) = \phi_C + \vec{O}C \times L = \bar{I}_C \omega$$

- Spatial Momentum: h

$$\phi_O = \phi_C + \vec{O}C \times L$$

Coordinate free

$$h = \begin{bmatrix} \phi \\ L \end{bmatrix} \in \mathbb{R}^6$$



Change Reference Frame for Momentum

- Spatial momentum transforms in the same way as spatial forces:

${}^A h = {}^A X_C^* {}^C h$

$A_{T_c} = ({}^A R_c, {}^A p_c)$

$${}^C h = \begin{bmatrix} {}^C \phi_{0c} \\ {}^C L \end{bmatrix}$$

$${}^A h = \begin{bmatrix} {}^A \phi_{0A} \\ {}^A L \end{bmatrix}$$

$${}^A L = \underbrace{{}^A R_c}_{3 \times 3} {}^C L \quad \left| \begin{array}{l} 3 \times 1 \\ 3 \times 1 \end{array} \right.$$

↔ coordinate free

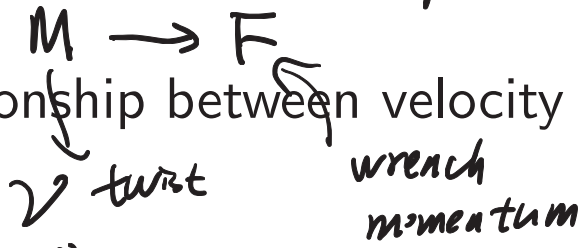
$$\phi_{0A} = \phi_{0c} + (\vec{0}_A \times L)$$

\Rightarrow ${}^A \phi_{0A} = \underbrace{{}^A R_c}_{3 \times 3} {}^C \phi_{0c} + {}^A R_c (-p_A \times {}^C L)$

$$= \begin{bmatrix} {}^A R_c & {}^A R_c [-p_A] \end{bmatrix} \begin{bmatrix} {}^C \phi_{0c} \\ {}^C L \end{bmatrix} \Rightarrow \boxed{{}^A h = {}^A X_C^* {}^C h} \in \mathbb{R}^6$$

Spatial Inertia

think about inertia matrix as mapping



- Inertia of a rigid body defines linear relationship between velocity and momentum.

- Spatial inertia \mathcal{I} is the one such that

$$\begin{array}{ccc}
 & & 6 \times 6 \\
 & \swarrow & \\
 h = \mathcal{I} \mathcal{V} & & \\
 \swarrow & \nwarrow & \\
 6 \times 1 & & 6 \times 1
 \end{array}$$

- Let $\{C\}$ be a frame whose origin coincide with CoM. Then

In this case, we know

$${}^c \mathcal{V} = \begin{bmatrix} {}^c \omega \\ {}^c v_c \end{bmatrix}, \quad {}^c v_{com} = {}^c v_c \Rightarrow {}^c \mathcal{H} = m {}^c v_c$$

$${}^c \mathcal{I} = \begin{bmatrix} {}^c \bar{I}_c & 0 \\ 0 & m I_3 \end{bmatrix}$$

\downarrow 3×3 identity \rightarrow ${}^c \mathcal{I}$

$${}^c \phi_c = {}^c \bar{I}_c {}^c \omega$$

$${}^c h = \begin{bmatrix} {}^c \bar{I}_c {}^c \omega \\ m {}^c v_c \end{bmatrix} = \begin{bmatrix} {}^c \bar{I}_c & 0 \\ 0 & m I_{3 \times 3} \end{bmatrix} {}^c \mathcal{V}$$

3×3 identity matrix

Spatial Inertia



- Spatial inertia wrt another frame $\{A\}$:

$$\underline{{}^A h} = \underline{{}^A R_C} \underline{{}^C h} = \underline{{}^A X_C}^* \underline{{}^C h} = \underline{{}^A X_C}^* \underline{{}^C I} \underline{{}^C v} = \underline{{}^A X_C}^* \underline{{}^C I} \underline{{}^C X_A} \underline{{}^A v}$$

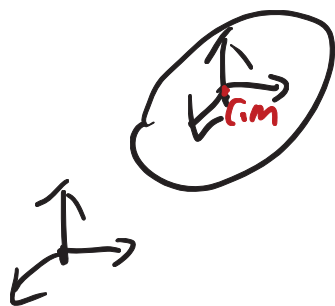
${}^A I = {}^A X_C^* \underline{{}^C I} \underline{{}^C X_A}$

when $\{A\}$ has same orientation of $\{C\}$ frame



- Special case: ${}^A R_C = I_3$

we know ${}^A X_C = \begin{bmatrix} I_3 & 0 \\ [{}^A p_C] & I_3 \end{bmatrix} \Rightarrow$



$$\underline{{}^A I} = \begin{bmatrix} \underline{{}^C I} + m [{}^A p_C] [{}^A p_C]^T & m [{}^A p_C] \\ m [{}^A p_C] & m I_{3 \times 3} \end{bmatrix}$$

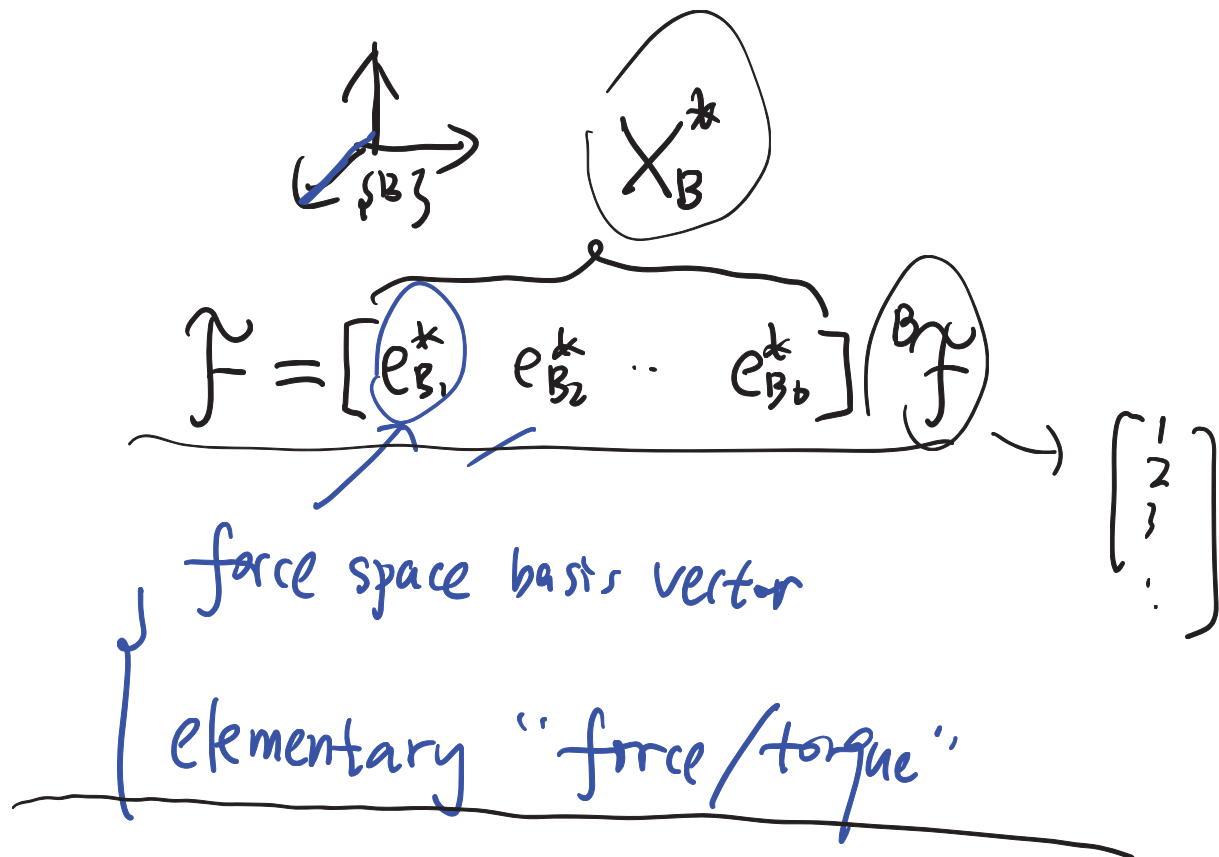
Outline

- Spatial Acceleration

- Spatial Force (Wrench)

- Spatial Momentum

- Newton-Euler Equation using Spatial Vectors



$$\dot{\mathcal{F}} = \dot{X}_B^* \mathcal{F} + X_B^* \underbrace{(\mathcal{F})'}_{\mathcal{F}^o}$$

It turns out (if $\{B\}$ has velocity v_B)

Cross Product for Spatial Force and Momentum

Assume frame \underline{A} is moving with velocity ${}^A \mathcal{V}_A$

- $${}^A \left[\frac{d}{dt} \mathcal{F} \right] = \frac{d}{dt} ({}^A \mathcal{F}) + {}^A \mathcal{V}_A \times {}^A \mathcal{F}$$

\downarrow coordinate-free \leftarrow ${}^A \mathcal{F}$: apparent

- $${}^A \left[\frac{d}{dt} h \right] = \frac{d}{dt} ({}^A h) + {}^A \mathcal{V}_A \times {}^A h$$

Fact: $[\mathcal{V}_{x^*}] = -[\mathcal{V}_x]^T$

$$\dot{\mathcal{F}} = X_B^* \dot{\mathcal{F}}^0 + [\mathcal{V}_B x^*] X_B^* \mathcal{F}$$

then: $\dot{e}_{Bi}^* = \mathcal{V}_B x^* e_{Bi}^*$

where " x^* " defined as

$$\mathcal{V} = \begin{bmatrix} w \\ v \end{bmatrix}, \quad \mathcal{F} = \begin{bmatrix} n \\ f \end{bmatrix}$$

$$\mathcal{V} x^* \mathcal{F} \triangleq \begin{bmatrix} w \times n + v \times f \\ w \times f \end{bmatrix}$$

or equivalently

$$[\mathcal{V} x^*] = \begin{bmatrix} [w] & [v] \\ 0 & [w] \end{bmatrix}$$

$b \times b$

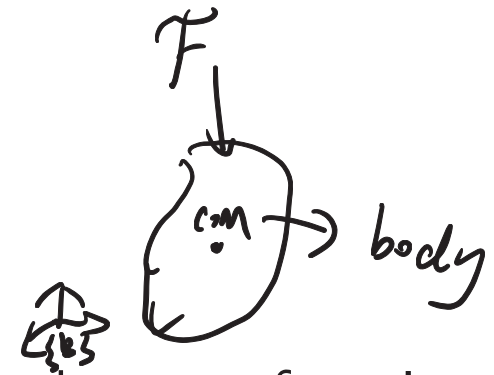
$$\Rightarrow \dot{X}_B^* = [\mathcal{V}_B x^*] X_B^*$$

Newton-Euler Equation

- Newton-Euler equation:

net external wrench

$$\mathcal{F} = \left(\frac{d}{dt} h \right) = \mathcal{I}A + \mathcal{V} \times^* \mathcal{I}\mathcal{V}$$



- Adopting spatial vectors, the Newton-Euler equation has the same form in any frame

$${}^B \tilde{\mathcal{F}} = {}^B \mathcal{I} {}^B A + ({}^B \mathcal{V}) \times^* {}^B \mathcal{I} ({}^B \mathcal{V}) \quad (\text{even when } \{B\} \text{ is away from COM})$$

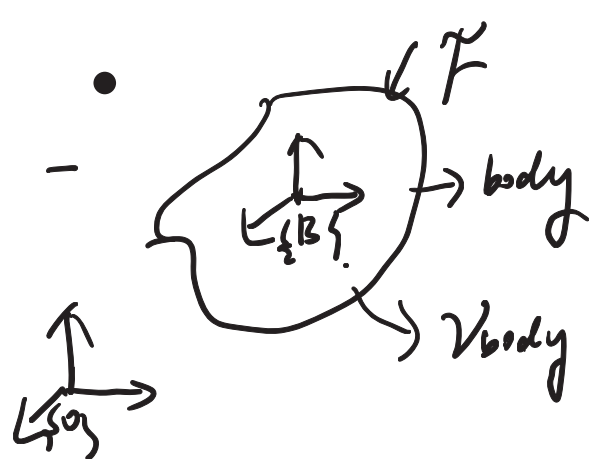
$${}^B \tilde{\mathcal{F}} = {}^B \left(\frac{d}{dt} h \right) = {}^B \left(\frac{d}{dt} (\mathcal{I}\mathcal{V}) \right) = {}^B (\mathcal{I}A + \dot{\mathcal{I}}\mathcal{V})$$

Let's work with inertia frame $\{i\}$
to derive the NE-equation.

$$= \mathcal{I}A + \mathcal{V} \times^* \mathcal{I}\mathcal{V}$$

$\mathcal{I}A$ is due to \mathcal{V} (velocity) is changing
 $\mathcal{V} \times^* \mathcal{I}\mathcal{V}$ Accounts for the fact that inertia is moving

Derivations of Newton-Euler Equation



Assume: $\{B\}$ attached to the body
 $\Rightarrow v_B = v_{body}$, I_B is constant

$$\begin{aligned} \frac{d}{dt}({}^0h) &= \frac{d}{dt}({}^0I v) = \dot{{}^0I} v + {}^0I \dot{A} \\ &= \frac{d}{dt}({}^0X_B^* I^B X_0) v + {}^0I \dot{A} \\ &= (\dot{{}^0X_B^*} I^B X_0 v + {}^0X_B^* I^B \dot{X}_0 v) + {}^0I \dot{A} \quad \text{where } {}^0v = v_B \\ &= \underbrace{[v_B X^*]}_{} {}^0X_B^* I^B X_0 v - \cancel{{}^0X_B^* I^B X_0 [v_B X^*]} v + {}^0I \dot{A} \\ &= \boxed{[v_B X^*] {}^0I v + {}^0I \dot{A}} \\ &= {}^0I \dot{A} + v_B X^* \dot{{}^0I} v \end{aligned}$$

Note: $\dot{{}^0X_B} = [v_B X^*] {}^0X_B$, $({}^0X_B I^B X_0) = I \Rightarrow \dot{{}^0X_B} I^B X_0 + {}^0X_B \dot{I}^B X_0 = 0 \Rightarrow \dot{I}^B X_0 = -{}^0X_B [v_B X^*]$

More Discussions

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More Discussions

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